Product Information

Introduction
Because of the phaseout of chlorofluorocarbon (CFC) refrigerants, environmentally acceptable replacements have been commercialized for use in new chillers and in chillers originally designed for use with CFCs. The “alternative” refrigerants have operating characteristics similar to those of CFCs, both to limit the design changes involved in manufacturing new chillers that use these new refrigerants and to reduce the cost of converting existing chillers from CFCs to them.

Chemours is now producing Freon™ 134a refrigerant as a replacement for CFC-12 in chillers, and is providing this new refrigerant to chiller manufacturers for use in new and existing chillers. Chemours has converted most of its own CFC-12 and R-500 chillers to Freon™ 134a and has replaced its other CFC-12 and R-500 chillers with new chillers operating on HCFC-123, Freon™ 134a, or HCFC-22.

Property comparisons of Freon™ 134a with CFC-12 are outlined in Table 1. The boiling point of the new refrigerant is close to that of CFC-12. This means that Freon™ 134a develops system operating pressures similar to CFC-12.

The environmental advantages of Freon™ 134a over CFC-12 are clearly shown by the ozone depletion potential (ODP) and global warming potential (GWP) values of the two compounds. Neither compound is flammable. The 1,000 ppm Allowable Exposure Limit (AEL) of Freon™ 134a means that this refrigerant is expected to have similar toxicity characteristics as CFC-12 and the other CFC refrigerants.

General Considerations
In general, alternative refrigerants cannot be simply “dropped into” a system designed to use CFCs.

Table 1, Property Comparisons

<table>
<thead>
<tr>
<th></th>
<th>CFC-12</th>
<th>Freon™ 134a</th>
</tr>
</thead>
<tbody>
<tr>
<td>Boiling Point, °C (°F)</td>
<td>-30 °C (–21.6 °F)</td>
<td>-26.1 °C (–14.9 °F)</td>
</tr>
<tr>
<td>Flammability</td>
<td>None</td>
<td>None</td>
</tr>
<tr>
<td>Exposure Limit, ppm (V/V)</td>
<td>1,000 TLV*</td>
<td>1,000 AEL**</td>
</tr>
<tr>
<td>Ozone Depletion Potential</td>
<td>1.0</td>
<td>0.0</td>
</tr>
<tr>
<td>Global Warming Potential (100 yr. ITH)</td>
<td>8,500</td>
<td>1,300</td>
</tr>
</tbody>
</table>

*A Threshold Limit Value (TLV), established for industrial chemicals by the American Conference of Governmental Hygienists, is the time-weighted average concentration of an airborne chemical to which workers may be exposed during an 8-hour workday 40 hours per week for a working lifetime.

**An Acceptable Exposure Limit (AEL) is the recommended time-weighted average concentration of an airborne chemical to which nearly all workers may be exposed during an 8-hour workday 40 hours per week for a working lifetime without adverse effect, as determined by Chemours for compounds that do not have a TLV.

Depending on the specifics of the machine, materials may need to be replaced and, in many cases, the compressor will need to be modified. When converting a chiller from a CFC to Freon™ 134a, the lubricant will need to be replaced. Maintenance records should list any modifications that have been made to original system components. Also, the equipment manufacturer should be consulted regarding compatibility of system parts with the new refrigerant.

Performance Comparisons
As shown in Table 2, the performance characteristics of Freon™ 134a are similar to those of CFC-12. Freon™ 134a was initially thought to be slightly less efficient than CFC-12, based on models that did not take into account differences in heat transfer coefficients between the two refrigerants. Chillers converted to Freon™ 134a are performing about the same as they did on CFC-12.
Although a new chiller can be designed for Freon™ 134a, an existing chiller operating on CFC-12 will have to undergo some modifications to operate on the new refrigerant. The lubricant will need to be changed and the impeller speed increased 10–15% or replaced with impellers suitable for Freon™ 134a. Experience to date with retrofit of CFC-12 and R-500 chillers to Freon™ 134a is discussed later in this bulletin.

**Table 2.** Typical Retrofit Performance Ranges of Freon™ 134a versus CFC-12

<table>
<thead>
<tr>
<th></th>
<th>+2 to –10%</th>
<th>+2 to –8%</th>
</tr>
</thead>
<tbody>
<tr>
<td>Capacity</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Coefficient of Performance</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Evaporator Pressure Difference</td>
<td>0 to –3 psi 0 to –0.2 bar</td>
<td></td>
</tr>
<tr>
<td>Condenser Pressure Difference</td>
<td>+15 to +25 psi +1 to +1.7 bar</td>
<td></td>
</tr>
<tr>
<td>Discharge Temperature Difference</td>
<td>0 to –10 °F 0 to –5.6 °C</td>
<td></td>
</tr>
</tbody>
</table>

Note: Actual performance will depend on the specific equipment and operating conditions used.

### Materials Compatibility

When converting from CFC-12 to Freon™ 134a, there are several factors that must be considered, most notably chemical compatibility. Table 3 lists the prominent considerations that must be addressed.

A primary consideration in chemical compatibility is finding a stable lubricant. In conventional refrigeration and air conditioning applications, there is a very slow reaction between the lubricant and refrigerant, which generates HCl and carbon compounds. Over the past 50 years, lubricants have been developed that are practically non-reactive with CFC refrigerants. Lubricants have now been developed that have acceptable stability with Freon™ 134a.

Common construction materials, such as copper, steel, and aluminum, are suitable for CFC refrigerants. However, in some circumstances, catalysts for the lubricant/refrigerant reaction, such as AlCl$_3$ and AlF$_3$, can be formed. The chemical stabilities of copper, steel, and aluminum have been tested and confirmed as acceptable for use with Freon™ 134a and lubricants.

Acceptable plastics and elastomers have been found for use with existing CFC refrigerants. However, an elastomer or plastic that is acceptable with one refrigerant may not perform well with another. For this reason, elastomers should be qualified on an application by application basis. Testing with Freon™ refrigerants shows that there will be no one family of elastomers or plastics that will work with all the alternative refrigerants. The results of using improper materials may include swelling, extraction of plasticizers and fillers, and changes in mechanical properties due to extraction and exposure to refrigerants. Table 4 provides a comparison of elastomer compatibility for CFC-12 versus Freon™ 134a.

**Table 3.** Chemical Compatibility Considerations

**Lubricants**
- Chemical reactivity with Freon™ 134a
- HCl, carbon compounds

**Metals**
- Chemical reactivity with Freon™ 134a
- Catalyst formation at high temperatures (AlCl$_3$, AlF$_3$)

**Elastomers**
- Swelling
- Mechanical property changes due to refrigerant/lubricant exposure
- Permeation of Freon™ 134a

**Plastics**
- Mechanical property changes due to refrigerant/lubricant exposure

### Lubricant/Refrigerant Relationships

In many refrigeration and air conditioning systems, some lubricant escapes from the compressor discharge area and circulates through the system with the refrigerant.

Lubricants used with CFC-12 are fully miscible over the range of expected operating conditions, easing the problem of getting the lubricant to flow back to the compressor. Refrigeration systems using CFC-12 take advantage of this full miscibility when considering lubricant return. Refrigerants with little or no chlorine may exhibit less miscibility with many lubricants. When such refrigerants are tested with lubricants, critical miscibility curves show that the refrigerant and lubricant tend to separate at lower temperatures.

Another consideration of refrigerant/lubricant solutions is lubricity. Once a combination with acceptable solubility is found, the lubricant’s ability to perform its primary function of lubricating compressor components must be established. If a miscible lubricant is found that has inadequate lubricity, additives can be included to improve lubrication. However, these lubricity enhancers can create solubility problems or introduce chemical reactions between the refrigerant and lubricant.
Freon™ 134a Refrigerant

Table 4. Elastomer Compatibility of Freon™ 134a

<table>
<thead>
<tr>
<th></th>
<th>CFC-12</th>
<th>Freon™ 134a</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>25 °C (77 °F)</td>
<td>80 °C (176 °F)</td>
</tr>
<tr>
<td>Adiprene L</td>
<td>1</td>
<td>5</td>
</tr>
<tr>
<td>Buna N</td>
<td>1*</td>
<td>0*</td>
</tr>
<tr>
<td>Buna S</td>
<td>3</td>
<td>4</td>
</tr>
<tr>
<td>Butyl Rubber</td>
<td>2</td>
<td>4</td>
</tr>
<tr>
<td>Hypalon 4B</td>
<td>1</td>
<td>0</td>
</tr>
<tr>
<td>Natural Rubber</td>
<td>4</td>
<td>5</td>
</tr>
<tr>
<td>Neoprene W</td>
<td>0*</td>
<td>1*</td>
</tr>
<tr>
<td>Nordel Elastomer</td>
<td>2*</td>
<td>2*</td>
</tr>
<tr>
<td>Silicone</td>
<td>5</td>
<td>5</td>
</tr>
<tr>
<td>Thoikol FA</td>
<td>1</td>
<td>1</td>
</tr>
<tr>
<td>Viton™ A</td>
<td>5</td>
<td>5</td>
</tr>
</tbody>
</table>

*R: Recommend elastomer replacement after equipment teardown

The initial search for a candidate lubricant started with commercially available products. Table 5 shows solubilities of various refrigerant/lubricant combinations. Naphthenic, paraffinic, and alkylbenzene lubricants have very poor solubility with Freon™ 134a.

Initially, polyalkylene glycol (PAG) lubricants were used for chiller retrofits. PAG lubricants may be susceptible to chemical attack by chloride residue in a refrigeration system that previously contained CFC-12. The PAG or its moisture content may also affect hermetic motor materials. As a result, extensive cleaning of retrofits was required.

Polyol Ester Lubricants

Due to PAG lubricant concerns, the focus shifted to polyol ester lubricants that offer many of the same properties as PAGs. There are many types of polyol ester lubricants available today, and compressor original equipment manufacturers (OEMs) have specified different products based on individual testing. Contact the compressor or equipment OEM for more information on specific polyol ester lubricant recommendations.

In general, esters offer excellent solubility with HFC-134a, as shown in Table 5. In addition many of the esters are not highly sensitive to residual mineral oil concentration, an issue that made retrofits using PAGs difficult.

It is recommended that the mineral oil concentration be less than 10% for chilled water applications and less than 5% for low temperature applications, following a retrofit to an ester, primarily to prevent formation of a second lubricant phase when the refrigerant is changed to Freon™ 134a. Contact your equipment OEM for more information concerning lubricant handling procedures.

Chemours has screened many elastomers and plastics for compatibility with Freon™ 134a and polyol ester lubricants. Contact Chemours or your equipment OEM for more information.

Retrofitting Existing CFC-12 and R-500 Chillers

Background

The decision to retrofit CFC equipment with alternative refrigerants must be made based on the cost to retrofit versus the expected life of the equipment and the anticipated efficiency of the system after the retrofit. As discussed earlier, alternative refrigerants are similar to but not identical to the CFCs they are targeted to replace. The differences in properties must be considered carefully, because systems designed for CFCs may perform inefficiently or completely fail if improperly retrofitted with an alternative refrigerant.

Retrofit requirements can range from a minimum effort, such as replacing the lubricant, to significant equipment changes, such as replacing gears, impellers, or materials of construction located throughout the system.
The main point to remember is that a service technician cannot simply put an alternative refrigerant into a CFC system. The property data must be compared and the materials of construction reviewed. Then, changes recommended by the OEM must be made to ensure that the system will perform correctly and efficiently.

Chemours Retrofit Program

Working with major chiller manufacturers, Chemours has retrofitted its extensive inventory of CFC chillers to alternative refrigerants.

As a first step in this effort, the Company retrofitted open-drive and hermetic chillers in Chemours facilities, developing a general understanding of what is required to convert each manufacturer’s various models from CFC-12 or R-500 to Freon™ 134a. This program was then expanded and led to the conversion of essentially all Chemours CFC chillers of 20-ton (70-kW) capacity or higher to alternative refrigerants.

Field Experience

Case History #1

The first conversion of a CFC-12 chiller to Freon™ 134a was conducted at Chemours Sabine River Works in Orange, Texas in November 1989 on a 700-ton (2,460-kW) open-drive York unit with a 3,200-lb (1,455-kg) refrigerant charge. The compressor lubrication system and evaporator were flushed with CFC-11 to remove residual chlorinated oil before the system was charged with Freon™ 134a and a 300 SUS PAG lubricant. No modifications were made to the chiller before initial conversion to Freon™ 134a. The CFC-11 with residual oil was recovered and re-used in CFC-11 chillers on-site.

Initial performance testing showed a capacity loss of 13 to 17% versus CFC-12, along with an equivalent reduction of power requirement. It was also found that the compressor could not deliver sufficient discharge head to operate during summer when temperatures in the cooling water reach 32 to 34 °C (90 to 93 °F). The compressor did provide enough lift to operate during winter and was placed into service with Freon™ 134a, while plans were made to change out the gear set in the spring of 1990 to increase impeller rpm.

The chiller operated without incident over the winter of 1989–90, and the compressor was removed in March 1990 for disassembly inspection and gear replacement. The internal condition of the compressor was excellent with virtually no bearing wear, except for some marking on the thrust bearing that sometimes occurs during start-up in CFC-12 service. The gear set was replaced with one having an 8% higher rpm and the compressor was returned to service. Follow-up performance testing in May 1990 showed a 1 to 9% increase in capacity versus CFC-12 and a 1 to 8% increase in power consumption versus CFC-12. In short, the compressor performed better on Freon™ 134a and PAG oil than it had on CFC-12 and naphthenic oil. Also, the increase in impeller speed provided sufficient lift to permit summertime operation, and the chiller has been in service on Freon™ 134a ever since.

Case History #2

A second CFC-12/naphthenic oil chiller at Sabine, a Carrier open-drive unit, was converted to Freon™ 134a/PAG oil in December 1990. This was a 1,200-ton (4,224-kW) unit with an 8,000-lb (3,636-kg) charge of CFC-12. The gear
The external gear box was refitted with a higher ratio gear set to increase compressor speed by 13%. The system was then charged with 10,900 lb (4,955 kg) of Freon™ 134a and polyol ester oil. Initially a lower viscosity oil was installed in this unit. Unsatisfactory operating pressures were noted, and the oil was replaced with a higher viscosity oil. Preliminary testing found that the capacity was regained, but that energy consumption increased at full design capacity. Later experience has shown that the unit capacity has increased to 3,200 tons with energy consumption per ton better than the previous experience with CFC-12. Oil and refrigerant monitoring continued for several years with no problems.

Case History #5
In July 1992, a 2,000-ton (7,040-kW) open-drive Worthington 52EH CFC-12 chiller with naphthenic oil was converted to Freon™ 134a and a polyol ester oil at a Chemours chemical plant in Nashville, Tennessee. The unit provides chilled water for air conditioning and product cooling. The unit is unique because Worthington no longer produces chillers. The unit was installed in 1965 and had operated without overhaul for that entire period. The Worthington units in general are fitted with condensers that have design pressure ratings of 150 psig. In most retrofits, the pressure rating on the condenser will be inadequate for Freon™ 134a, and the condenser may have to be replaced. This application did not require condenser replacement. Application did not require condenser replacement. Initial computer evaluations indicated that a 4% speed increase would be required to achieve full capacity. The CFC-12 and mineral oil were removed from the system. The unit was opened and an overhaul was conducted. The compressor rotor was over-speed tested and re-installed. A single oil flush was performed with polyol ester oil. The unit was charged with 7,000 lb (3,181 kg) of Freon™ 134a refrigerant and started up. Preliminary testing confirmed the earlier expectation that no impeller speed increase would be needed to provide adequate discharge pressure during summer months, because this chiller was originally used with R-500 instead of CFC-12. Oil and refrigerant monitoring continued for several years with no problems.
Summary

Major chiller manufacturers now have Freon™ 134a chillers in commercial production. The retrofit technology developed over the past decade is now routinely used to retrofit CFC-12 and R-500 chillers to Freon™ 134a.

In conjunction with the chiller OEMs, Chemours continues to assist in educating the industry about how to handle this alternative refrigerant. This effort includes making people aware of the handling requirements of new refrigerants, the chemical compatibility requirements of oils and materials of construction, and the effects of conversion on chiller operating characteristics.

For more information about retrofitting CFC equipment for use with Freon™ refrigerants, contact the OEM or Chemours.